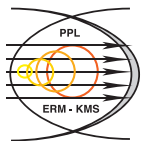





Ion cyclotron resonance heating modelling of JET, ITER and DEMO scenarios within the European Integrated Modelling (EU-IM) framework

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EUROfusion-IM Team




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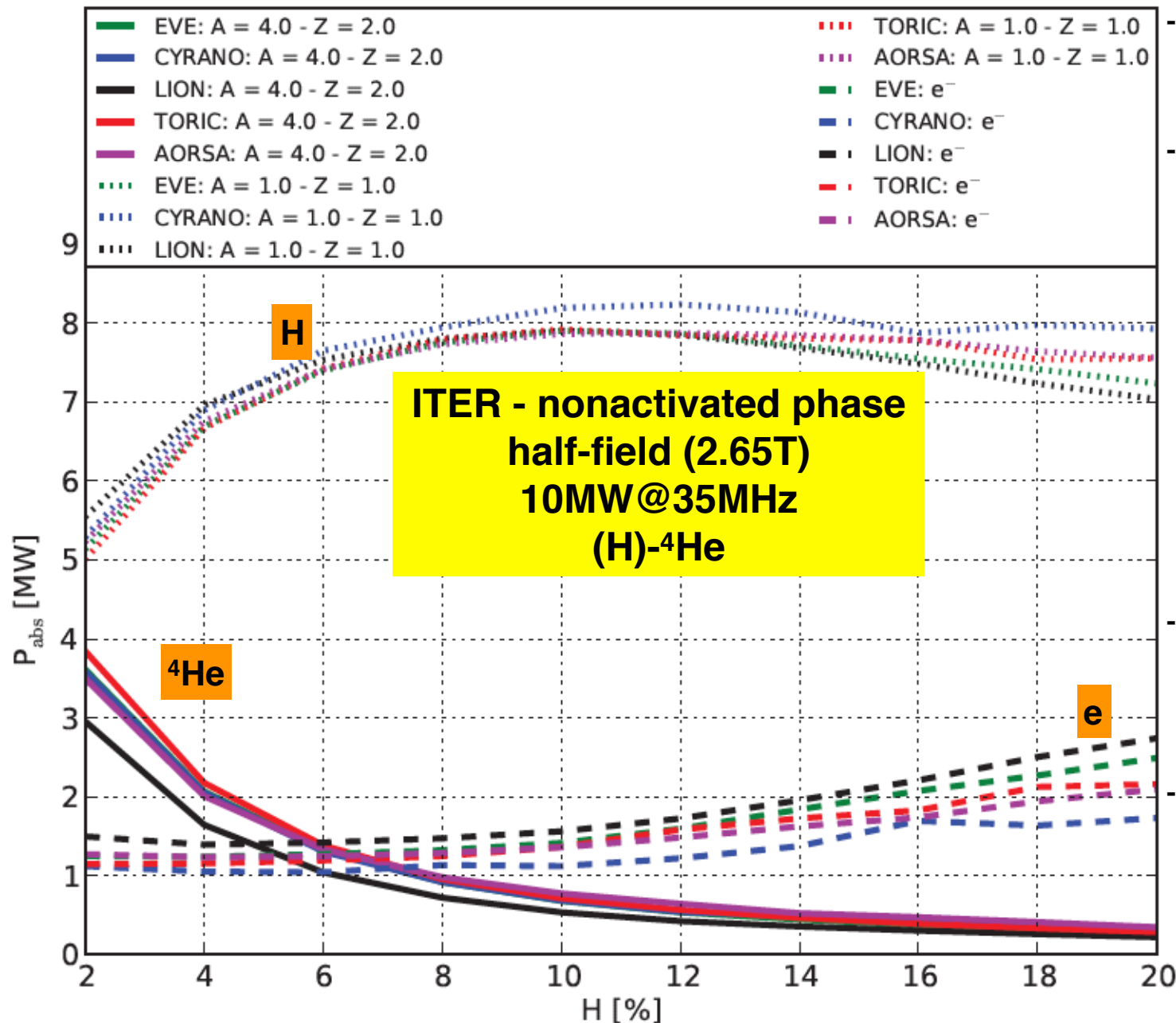
- Introduction & scope of this talk
- A few preliminary notes on ICRH in IMAS 
- Practical examples & tool demonstration (accent on ‘quick-n-dirty’ modelling; other ICRH related efforts in IMAS sprinkled here and there):
 - ICRH-NBI synergy in JET ‘baseline’ shot 92436
 - Optimising RF performance in preparation of JET D-T
 - Determining suitable ITER low B_0 field ICRH scenarios
 - Frequency choice of the DEMO ICRH system for the activated phase
- A quick note on the way forward
- Summary

Introduction & scope of this talk



- Theoretical/modelling **guidance** needed for preparation and analysis of experiments.
- “**Everything is coupled to everything else**” —> framework needed for modelling behaviour tokamak plasma allowing to zoom in on sub-aspects without user needing to know all details: **IMAS (Integrated Modelling & Analysis Suite)**, based on EUROfusion’s Integrated Modelling efforts & aligned with ITER IMAS! 
- Individual contributors focus on their field of expertise, delivering physics ‘**actors**’ that can be interconnected (via a graphical interface) to pass on required information. Both ‘quick & dirty’ & detailed codes available.
- Specific subtasks involving actors can be auto-defined and run. Biggest application so far: **ETS (European Transport Simulator)**
- Info stored in **shared, standardised data structure** with ‘shots’ and possibility to have independent time evolving runs stored and usable by other users.
- This talk illustrates what IMAS offers for modelling scenarios in which combined minority/majority/beam ICRH heating is instrumental.

IMAS = benchmarking + vali- & veri-fication platform



[R. Bilato et al., AIP Conference proceedings 1689, 060001 (2015)]

Easy comparison on basis of shared data files

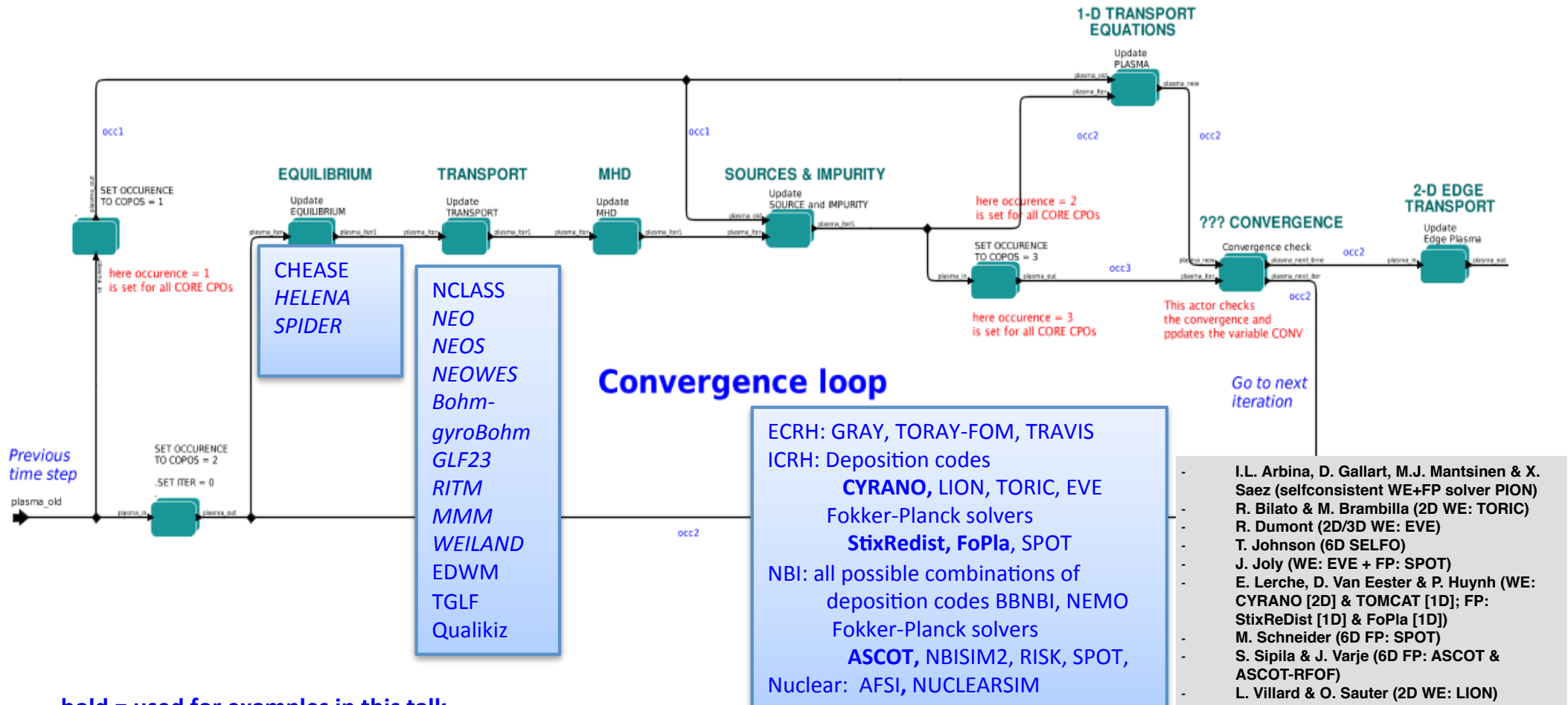
All WE codes share same input-output structure -> easily interchangeable (e.g. for testing scenarios requiring aspects only modeled in specific codes)

Various available 2D wave equation solvers show similar performance
Differences between predictions can be identified, helping to improve models.

ASCOT/TRANSP/Exp.:

[P. Sirén, J. Varje, H. Weisen, L. Giacomelli, submitted to J. Instrum. (2019)]

ETS: the European Transport Simulator



bold = used for examples in this talk

[P Strand, IAEA FEC 2018]

Self-consistent ICRH modelling ... or not



RF induced power density
Fokker-Planck equation

$$P_{\text{abs}} = \frac{\partial}{\partial t} \left[\int d\vec{v} d\vec{x} \varepsilon F_0 \right]_{\text{RF}} = \int d\vec{x} d\vec{v} \varepsilon \left. \frac{\partial F_0}{\partial t} \right|_{\text{RF}}$$

energy of particle population

$$= \frac{1}{2} \text{Re} \left\{ \int d\vec{x} d\vec{v} \varepsilon \nabla_{\vec{v}} \cdot \left[\frac{q}{m} [\vec{E} + \vec{v} \times \vec{B}]^* \int_{-\infty}^t dt' \frac{q}{m} [\vec{E} + \vec{v} \times \vec{B}] \cdot \nabla_{\vec{v}} F_0 \right] \right\}$$

RF diffusion operator

$$= -\frac{1}{2} \text{Re} \left\{ \int d\vec{x} d\vec{v} \frac{q}{m} [\vec{E} + \vec{v} \times \vec{B}]^* \cdot [\nabla_{\vec{v}} \varepsilon] \int_{-\infty}^t dt' \frac{q}{m} [\vec{E} + \vec{v} \times \vec{B}] \cdot \nabla_{\vec{v}} F_0 \right\}$$

RF induced power density
wave equation

$$= \frac{q}{2} \text{Re} \left\{ \int d\vec{x} d\vec{v} \vec{E}^* \cdot \vec{v} f_{\text{RF}} \right\} = \frac{1}{2} \text{Re} \left\{ \int d\vec{x} \vec{E}^* \cdot \vec{J}_{\text{RF}} \right\}$$

work done by field on particle population

RF perturbed distribution
 ε : energy
 F_0 : distribution

- **Fully self-consistent approach** [A. Kaufman, Phys. Fluids, 1972] tedious; **STILL not realised** ...
- In practice: WE & FP exchange **power density** rather than \underline{E} (exception FLR2 QL operator R.Bilato/ M.Brambilla: self-consistent truncated FLR2 approach).
- Often \neq species RF heated: min/maj/beam $\rightarrow \neq$ FP eqs. Coupling \neq FP eqs. forces review power balance:
 - Non-linear collision operator **conserves** particles, momentum, energy \rightarrow net input RF/NBI power requires net output; as $F_{o,e}$ converges most slowly: use 'electron reservoir' and **only integrate ion FP equations**.
 - **Equipartition** accounted for in FP but **reserved for transport equation**; to be taken out of FP equation (done solving for $P_{\text{RF}}=0$ & subtracting collisions)



Role of ICRH in D-T campaign:

- fusion ion heating
- high Z impurity chasing (ILW: W)
- ‘land’ the plasma

2 main roads to D-T operation:

- “Baseline”: (theoretical) performance scales with B_0 and I_p
- “Hybrid”: current profile tailoring - Can we make it stationary?

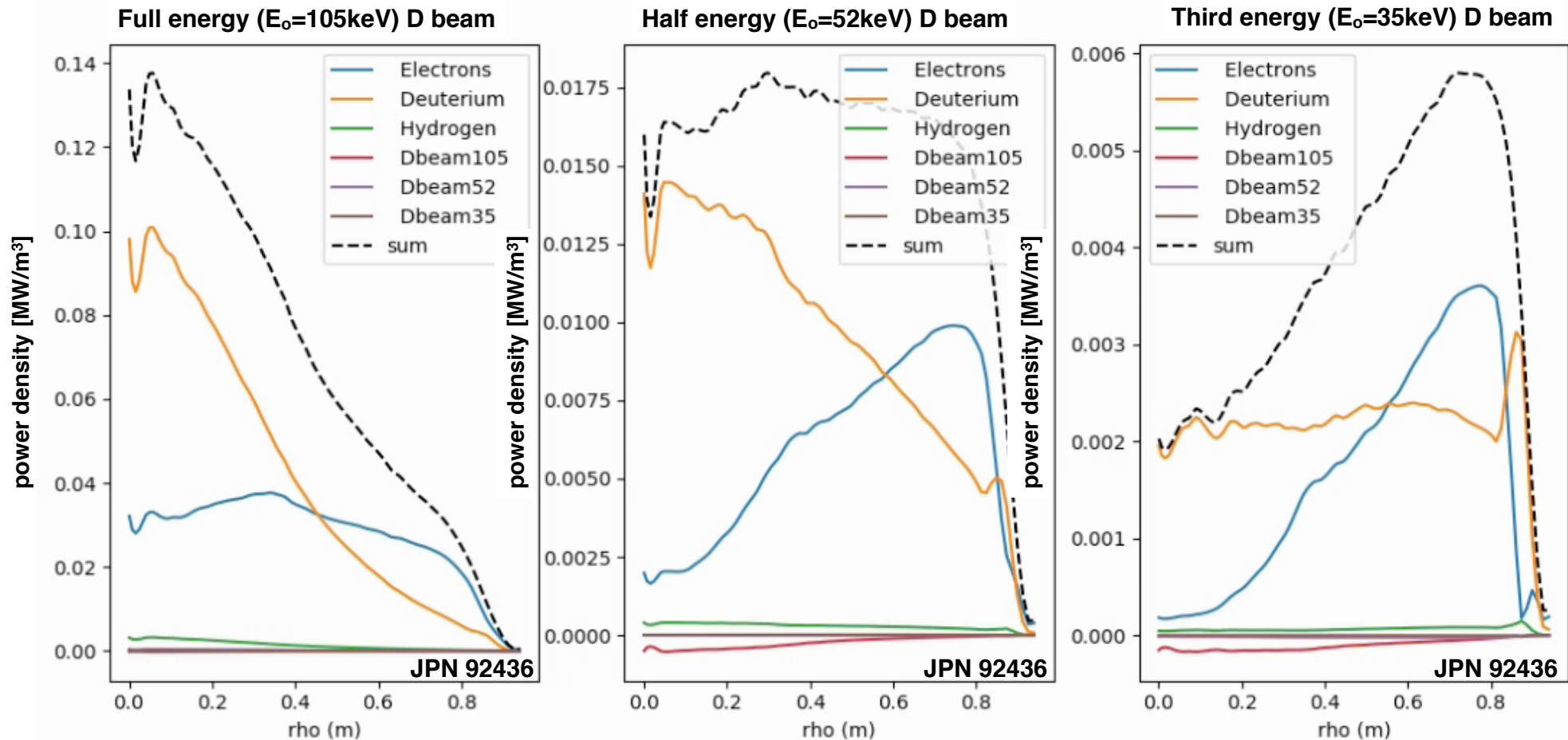
JET “work horse” scheme: [N=1 H] + [N=2 D] + [N=2 D_{NBI}]

Modelling baseline (H)-D-D_{NBI} JET shot 92436



sources computed by ASCOT code [E. Hirvijoki et al., Comput. Phys. Commun. 185 (2014) 1310]

[NBI-only collisional redistribution]

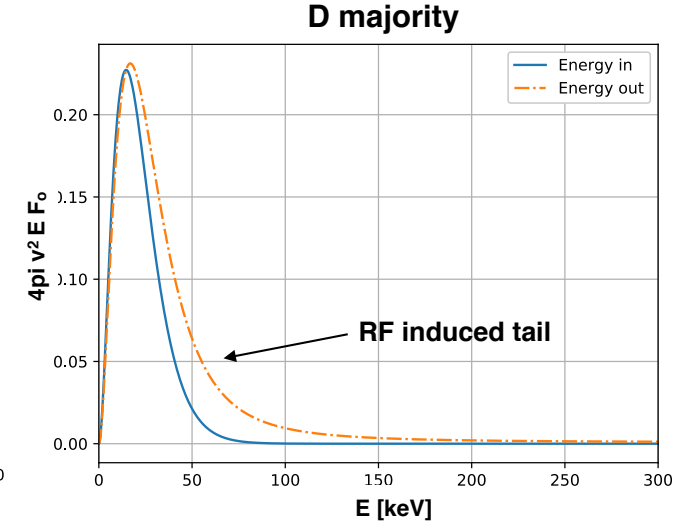
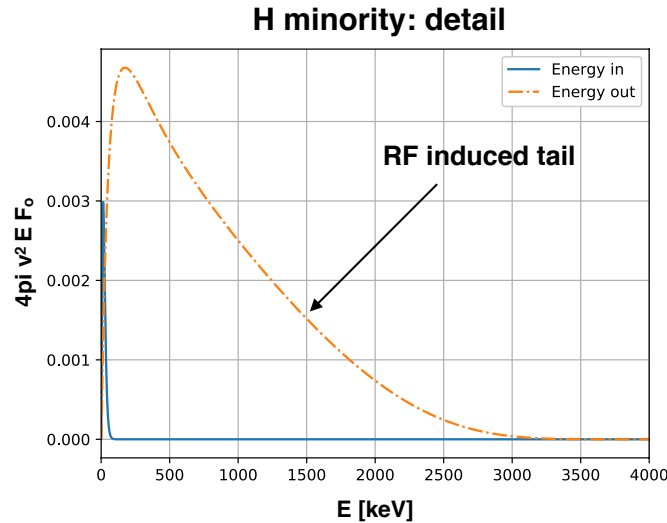
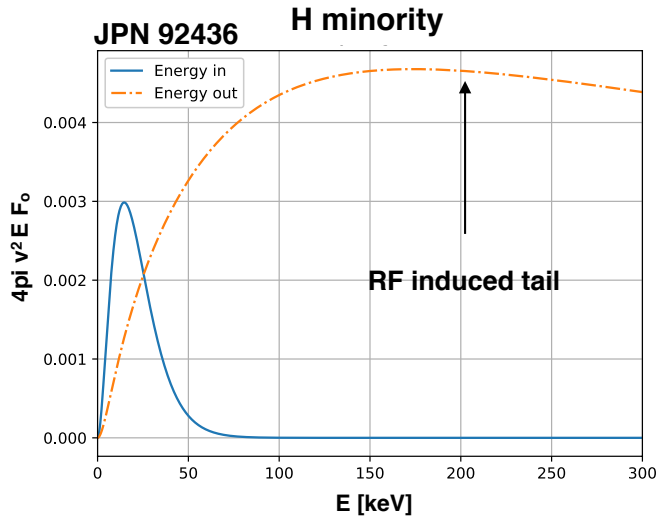


- high energy source peaks in core, low energy source peaks in edge
- dominant indirect bulk ion heating in core (high E_{crit}), electron heating near edge
- note: beam helps to 'preheat' target for ICRH (even when (Doppler shifted) RF absorption by NBI particles is irrelevant NBI impacts on RF heating)

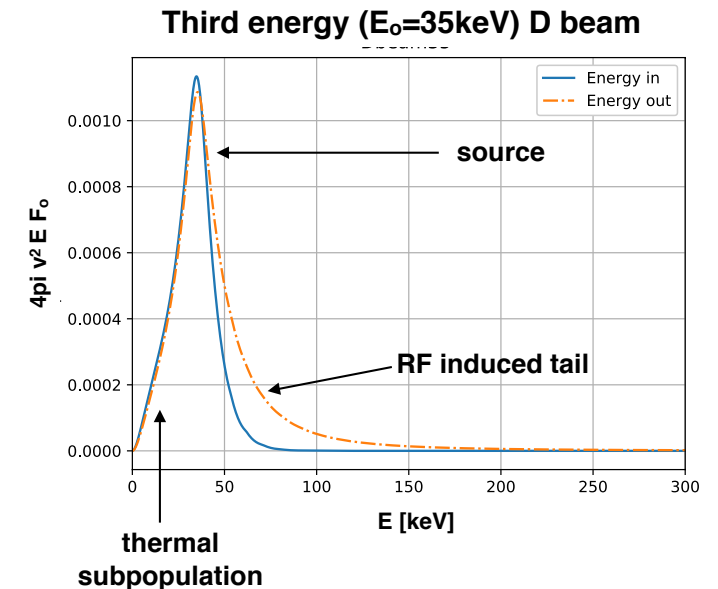
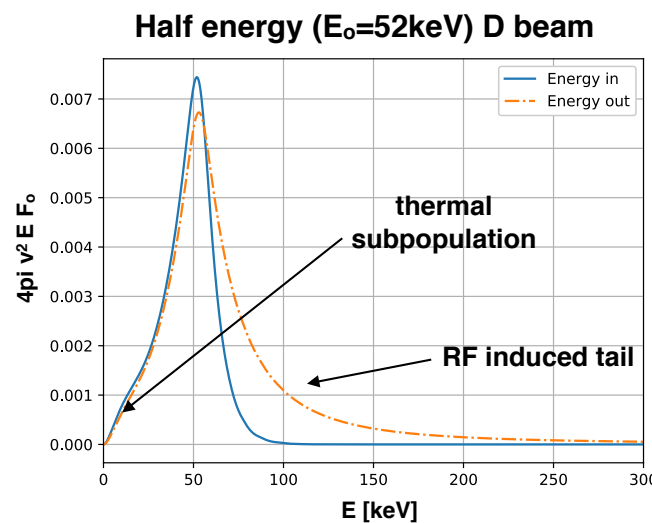
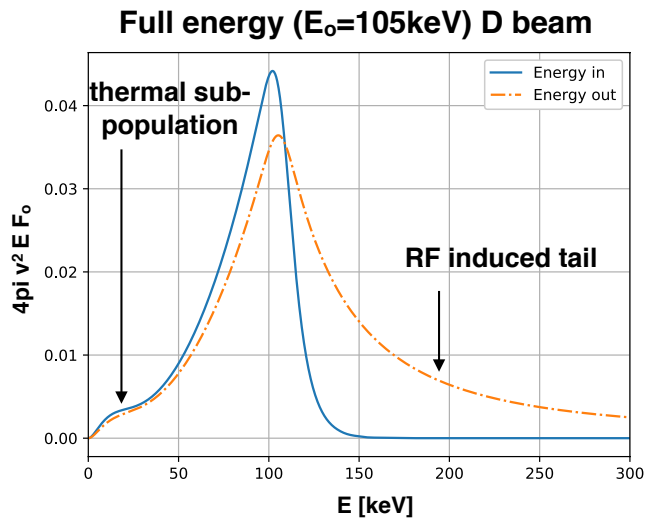
H minority N=1 heating:
thermal subpopulation affected;
high energy tail formed

Coupled FP eqs. solved for 5 i populations
(rho~13cm)

D majority N=2 heating:
thermal subpopulation ~ untouched;
high energy particles dominantly affected



D beam N=2 heating: thermal subpopulation ~ untouched; high energy particles dominantly affected

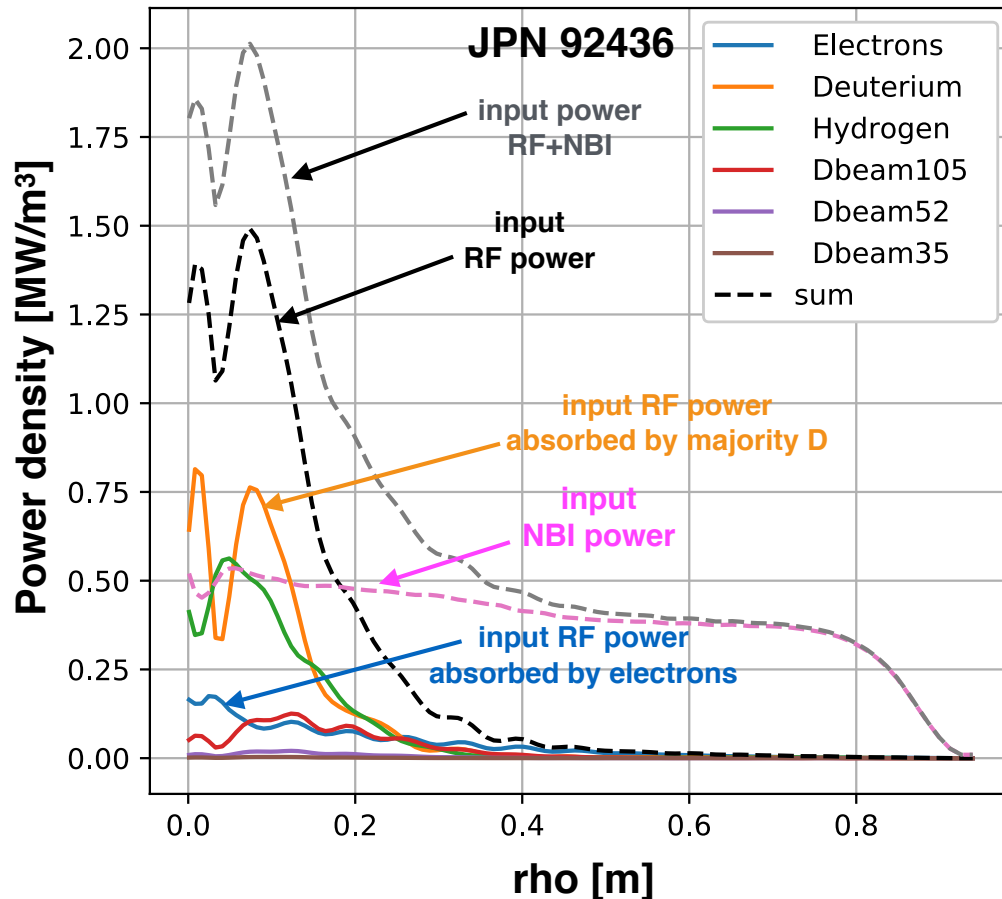


- High energy H tail formed
- D bulk preheated by NBI & forming tail at high energy (not shown)
- ICRH depopulates D NBI thermal region former high energy tail

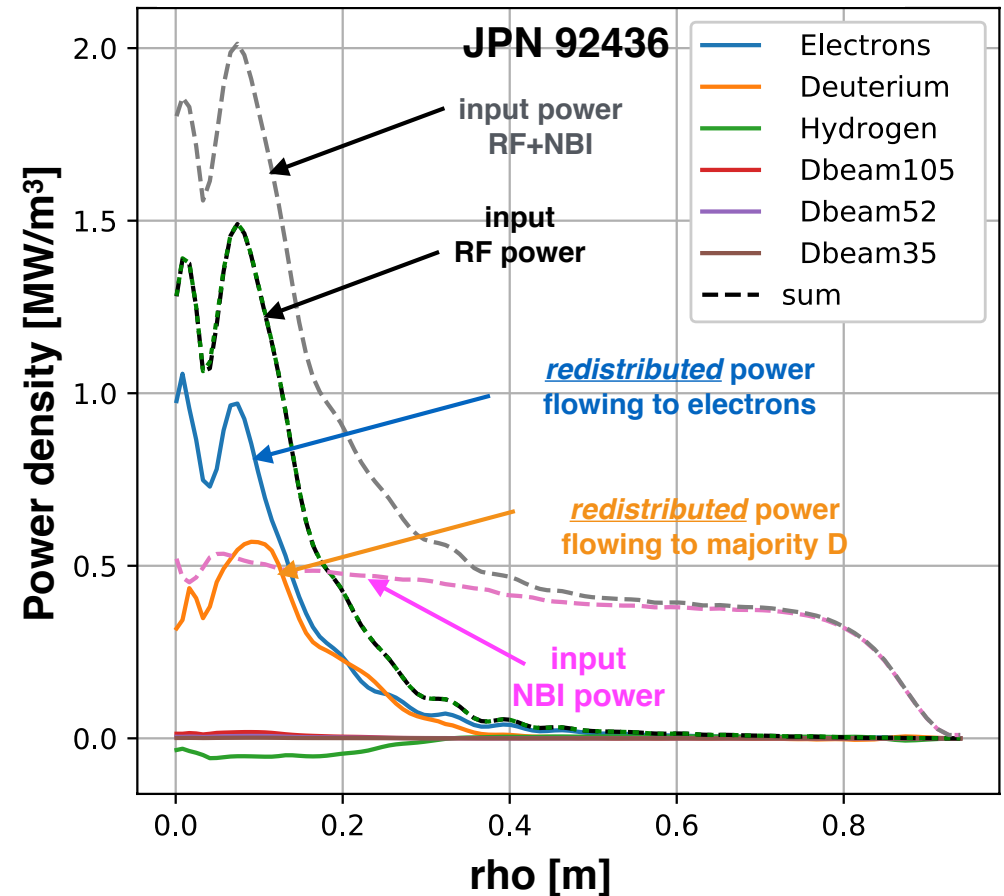
Power balance: direct & indirect heating



Direct wave & beam heating

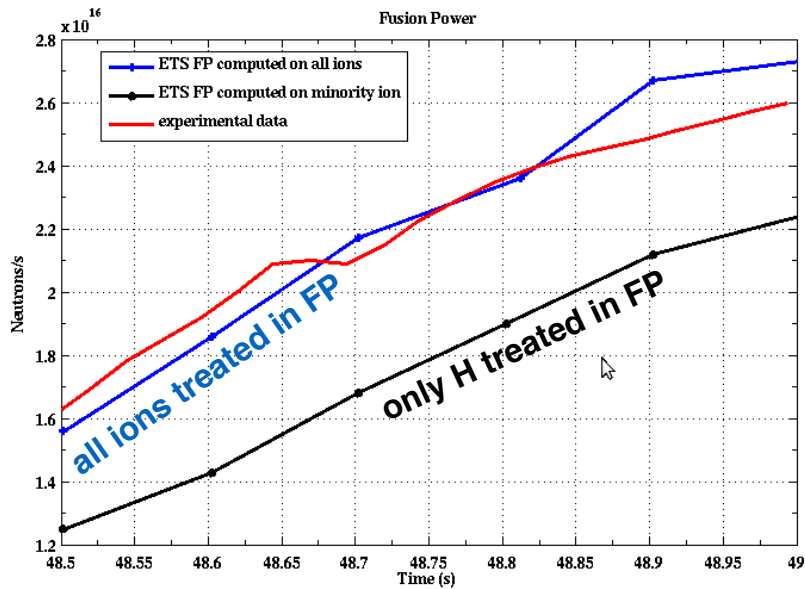
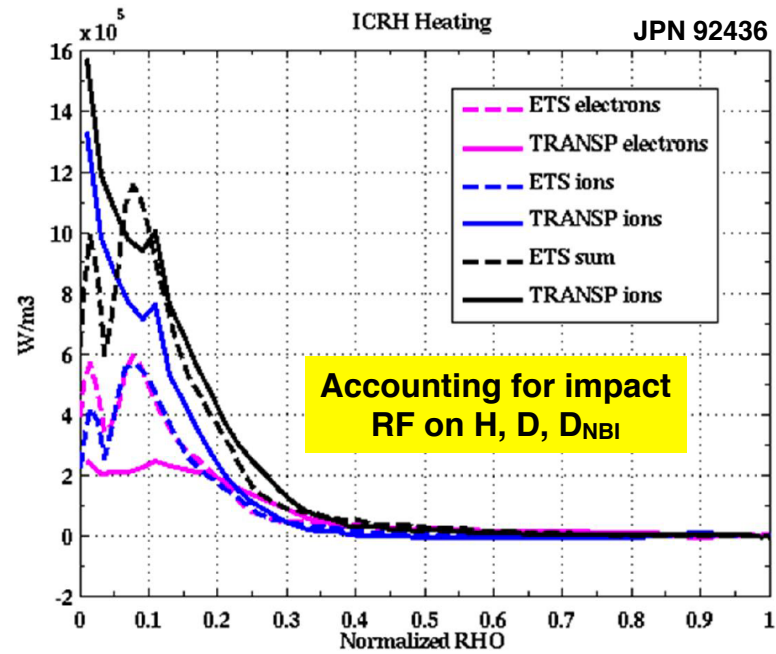
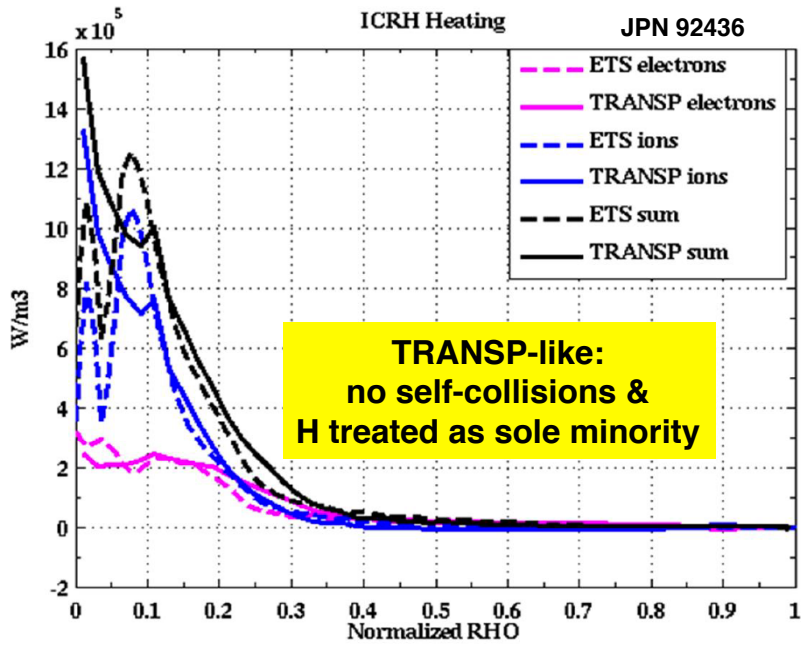


Indirect wave & beam heating



- electrons significantly indirectly heated in core region
- beams (heated at N=2) equally yield power electrons (but contribute to ion 'preheating')
- H minority dominantly heating electrons

ICRH - NBI synergy: minority \leftrightarrow all species FP

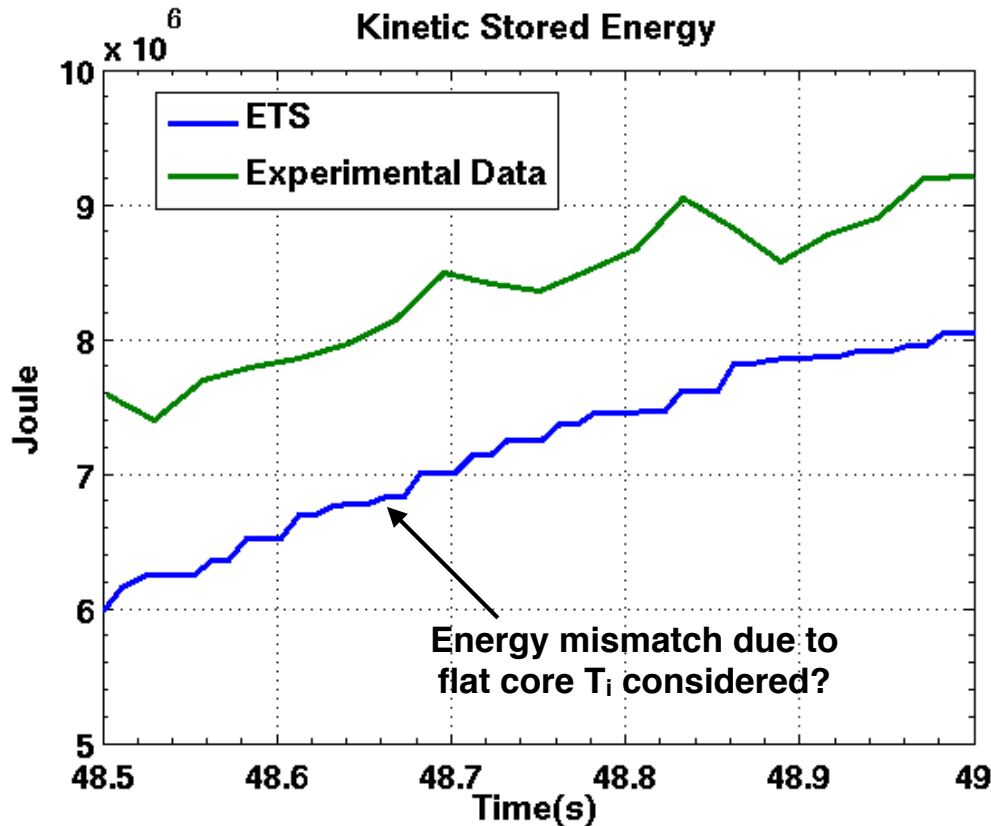


Neutron rate	ETS - H only in FF	ETS - all i in FP	Exp
D-D [10 ¹⁶ n/s]	1.20	1.60	
D-D _{nbi} [10 ¹⁶ n/s]	1.07	1.06	
D _{nbi} -D _{nbi} [10 ¹⁶ n/s]	0.04	0.04	
Total [10 ¹⁶ n/s]	2.32	2.70	2.60

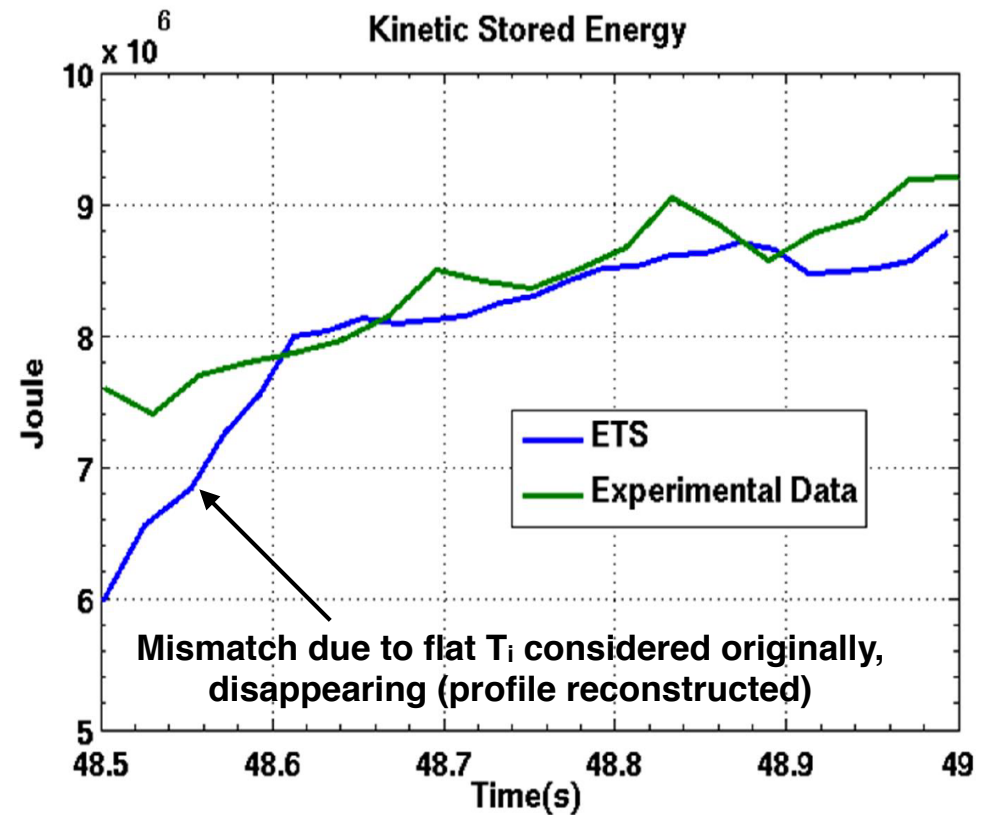
ICRH - NBI synergy: minority \leftrightarrow all species FP



interpretative



predictive



[Ph. Huynh, RF Power in Plasmas, Hefei, 2019]

Beyond 1D FP: Fast D with & without iterations EVE [R. Dumont] & SPOT [M. Schneider]

JET D_{NBI} : up to 20% of R_{DD} is due to synergy

& $T_{eff,NBI}$ increases from 40 to 60keV with 5MW of RF heating & 22MW D_{NBI}

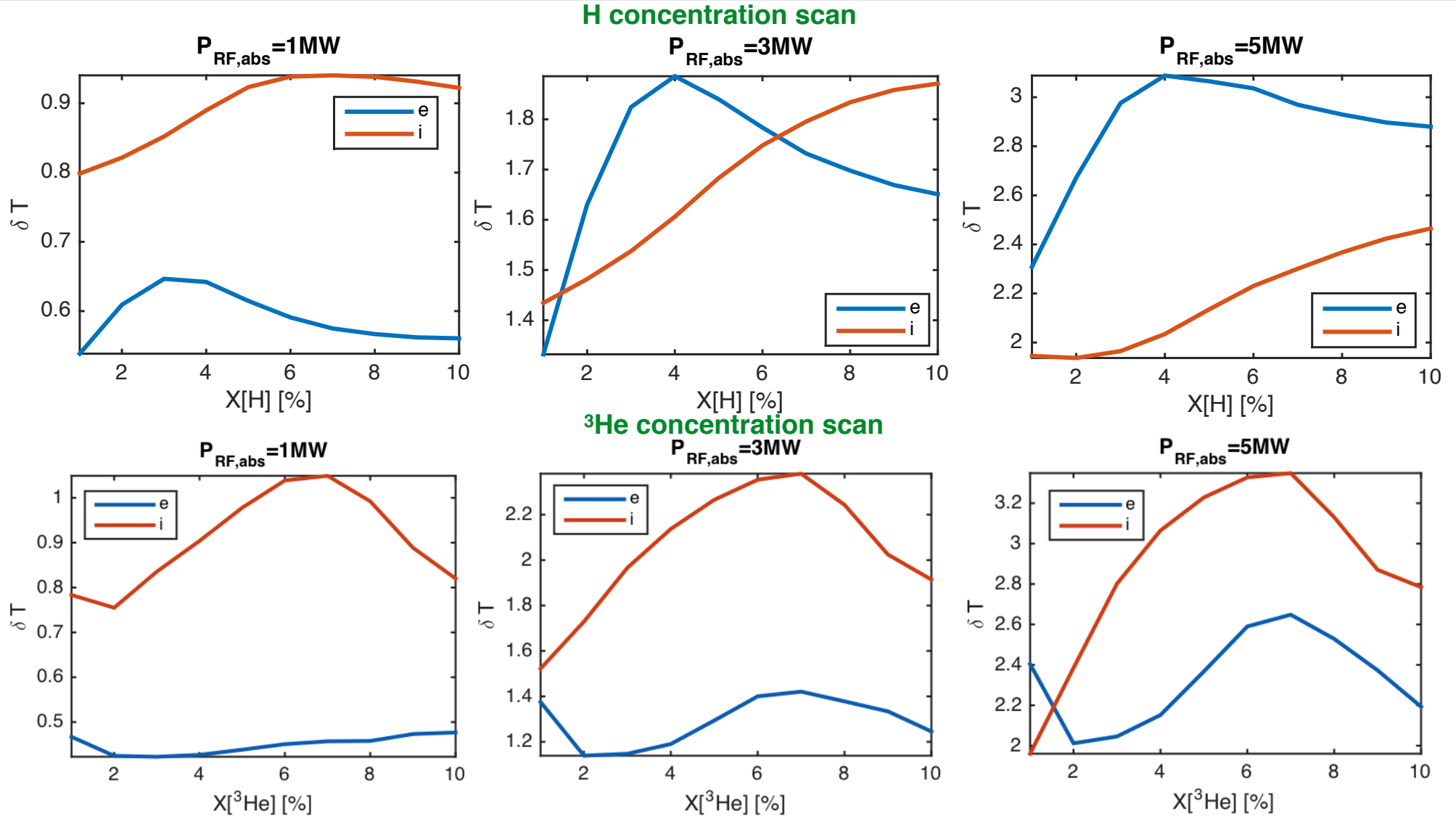
[J. Joly et al, Plasma Phys. Control. Fusion 61 (2019) 075017]

[J. Joly, PhD Thesis (in preparation)]

Role coupled power: JET baseline H & ^3He scan



Core temperature change due to RF



- Power increase \rightarrow temperature increase
- Low P_{RF} : $P_i > P_e$ both for H as ^3He (no high energy tails formed; energy $<$ critical energy)
- ^3He minority favours core ion heating; $P_e > P_i$ requires high power & low concentration
- Optimum ion heating @ $X[^3\text{He}] \sim 7\%$ for (^3He)-D; increasing with power in (H)-D
- Optimal e heating at $X[\text{H}] \sim 4\%$ for (H)-D and low $X[^3\text{He}]$ or $X[^3\text{He}] \sim 7\%$ for (^3He)-D
- At high power, using H minority favours e heating and ^3He favours i heating unless $X[^3\text{He}]$ small

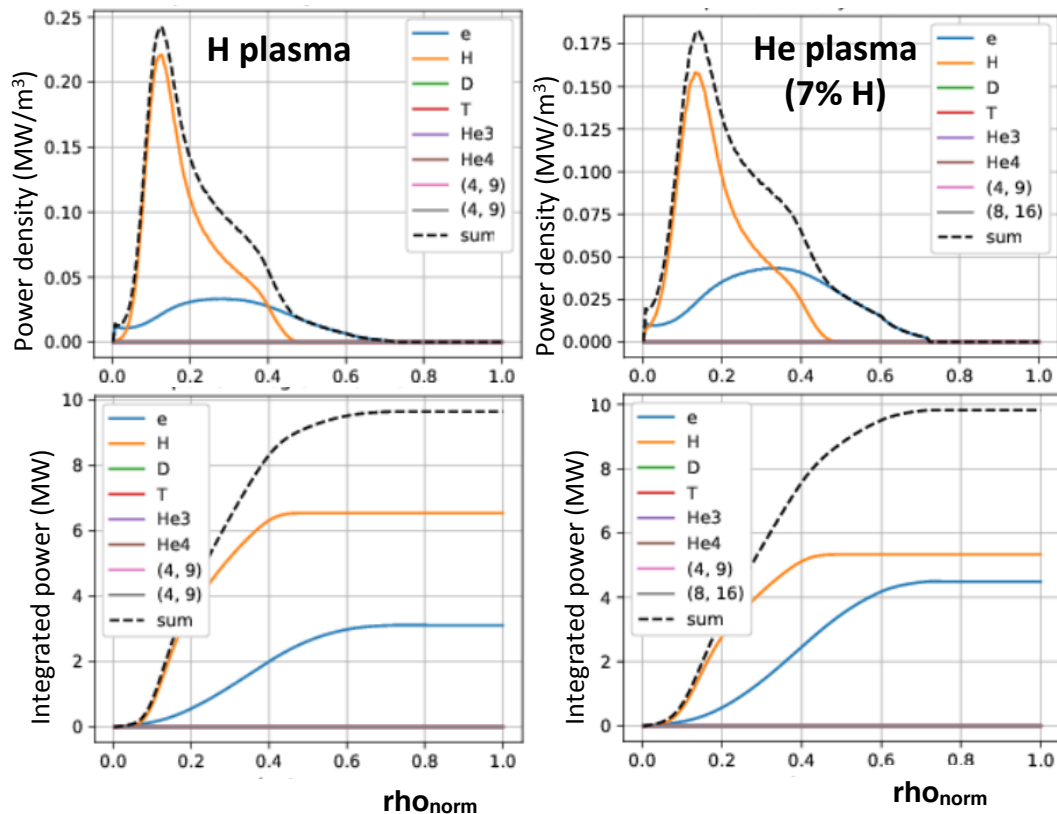
[simplified transport model used: coupled transport equations \neq species]



ITER: low B_0 field testing

METIS transport code used to provide kinetic profiles and equilibrium at 5MA/1.8T with 20MW EC and 10MW IC; $N_e=0.5N_{GW}$

TOMCAT code used to establish heating efficiency



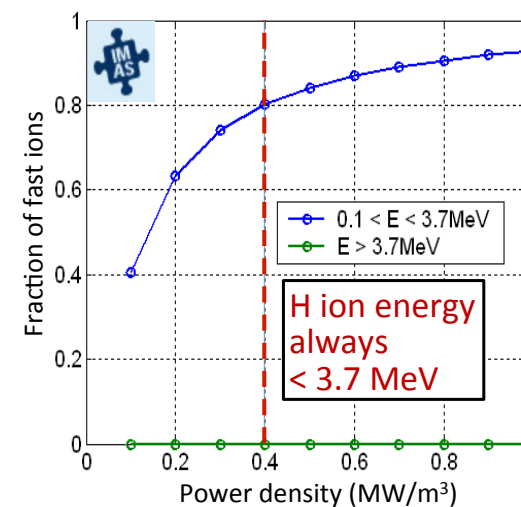
B_0 (T)	5.3	2.65	1.8	3	3.3		
I_p (MA)	15	7.5	5	8.5	9.5		
P_{AUX} (MW)	30				73		
Main ion	H	He	H	He	H	He	H
Te^0 (keV)	10	13	7.2	11	14	16	14
Ti^0 (keV)	12	16	6.0	12	7.0	8.0	10
ne^0 ($10^{19} m^{-3}$)	5.6	5.5	2.8	3.0	1.9	1.9	3.2
ni^0 ($10^{19} m^{-3}$)	5.4	2.9	2.7	1.7	1.8	1.0	2.2

- Best scheme: N=2 H heating in H and He plasmas ($f=52.5\text{MHz}$, $n_{tor}=40$)
- Very efficient single pass absorption (FLR scaling)
- More refined modelling done by PION code [L.-G. Ericsson et al, NF 33 (1993) 1037] installed under IMAS [I.L. Arbina, 46th EPS Conference on Plasma Physics, Milan (2019), P4-1079]

CYRANO & StixReDist codes used to provide input for assessment first orbit losses at 1.8T/5MA: for realistic power densities fast particles confined

[M. Schneider et al, Nucl. Fusion 59 (2019) 126014]

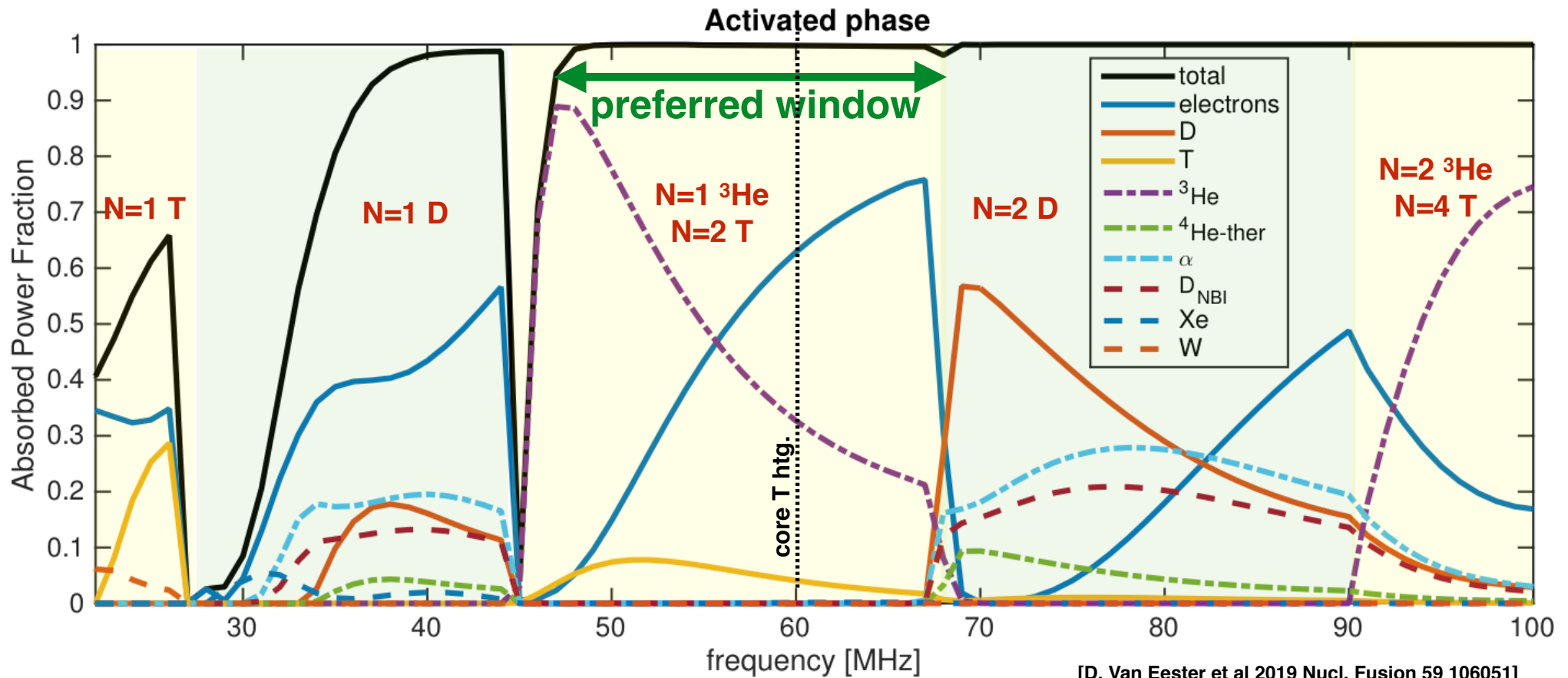
[M. Schneider - 27th IAEA FEC - Ahmedabad (India) - 22-27/10/18 - TH/6-1]



DEMO activated phase ICRH scenario assessment



DEMO-1 parameters : $R_0=9\text{m}$, $a_p=2.9\text{m}$, $B_0=5.855\text{T}$; $I_p=17.75\text{MA}$; $T_0=28\text{keV}$; $N_0=10^{20}/\text{m}^3$

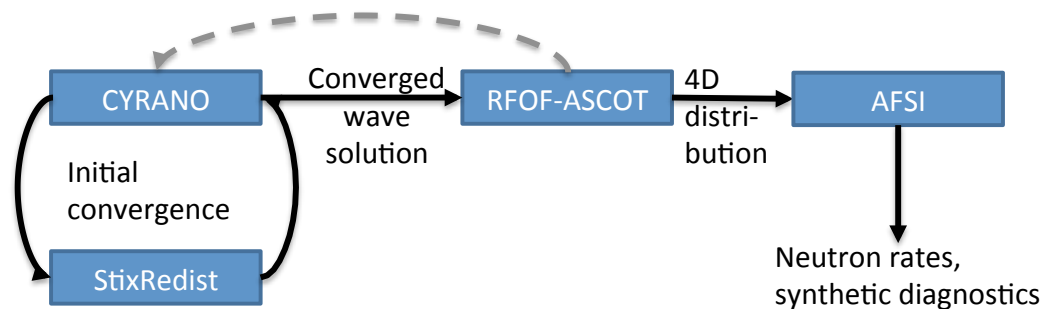


[D. Van Eester et al 2019 Nucl. Fusion 59 106051]

- Several possible windows depending on frequency chosen
- D fuel heating schemes spoiled by parasitic fusion born alpha particle absorption
- Significant e damping unavoidable
- ~100% SPA from $f \sim 50\text{MHz}$ (very high f window not examined)
- Proposed scheme identical as for ITER's activated phase (^3He)-D-T with small % of ^3He in early phase, D-T when steady burn reached
- $f=60\text{MHz}$ allows core fuel ion heating but e absorption exceeds ion absorption; nearby frequency optimal for CD (but low CD - comparable to other foreseen schemes - only: dedicated efforts needed e.g. Fisch proposal)



- Further improvement of models (e.g. RF kick operator in Monte-Carlo ASCOT to enable treating ICRH-NBI synergy)



- better integration
- more validation & benchmarking
- exploitation
- exploitation
- exploitation



- **IMAS** framework has **matured**
- EU-IM offers platform for code **validation** and **benchmarking**
- Gradually more intensive use yields further improved models; number of papers based on IMAS modelling steadily increasing
- Various ICRH-related examples based on IMAS tools discussed:
 - JET modelling **synergy** ICRH-NBI: baseline shot 9243 [good agreement with exp. parameters; need to include tail formation all RF heated species (min, maj, beam)]
 - JET modelling **H vs ³He** heating [good qualitative agreement with exp.; available RF power crucial factor]
 - ITER modelling: ICRH scenarios in early non-activated phase low B_o -field identified (**N=2 H**); first orbit losses assessment satisfactory
 - DEMO modelling of ICRH scenarios: opt for identical scenario as ITER (**N=1 ³He** & **N=2 T** in early phase discharge; **N=2 T** later)
- Further upgrading ongoing & needed but
- **IMAS tools are ready for exploitation!!**